



#### **Improving Radar Observation of Meteors using Compressed Sensing**

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### SESS



 Theory to guarantee solution of underdetermined set of equations

**Compressed Sensing** 

 Knowing that the solution is sparse or compressible provides uniqueness

#### Requirements

- Solution known to be sparse
- Measurements are "incoherent" (global)
- m ≥ O(s log n)

Number of measurements

Total number of variables

Sparsity = number of nonzero variables in solution

For more information: Candès and Wakin, "An Introduction to Compressive Sampling", IEEE Signal Processing Magazine, March 2008.

# SESS Compressed Sensing Solution



• **y = Ax** - Unknown signal vector

Measurement Linear system describing measurements vector

- Want to find sparsest solution that agrees with measurements
- Solve convex optimization problem:

$$x^* = \underset{\hat{x}}{\arg\min} \|x\|_1 \quad s.t. \quad \|y - A\hat{x}\|_2 \le \sigma$$

We use TFOCS software package for MATLAB



**Radar Model** 



$$y_q = \sum_{k=1}^{rm} s_{rq-k+1} \left( \sum_{p=0}^{n-1} e^{\frac{2\pi i p q}{n}} h_{p,k} \right)$$

- y<sub>q</sub> for q = 1,...,m is the sampled received signal (measurements)
- m is the number of samples
- $s_k$  for k = 1,...,b is a discrete phase shift modulation
- b is the number of bauds in the modulation
- r is the ratio of baud length to sampling period
- n is the number of frequencies
- h<sub>p,k</sub> are the reflectivity coefficients



Poker Flat, Barker-13 code, 10 us bauds, 5 us sampling period



Poker Flat, Barker-13 code, 10 us bauds, 5 us sampling period









### Conclusion



#### Advantages

- Complete noise filtering and easy signal identification
- Imaging with respect to Doppler frequency
- Easier to increase Doppler and range accuracy

#### Disadvantages

- Processing time
- Needs more development

#### Future Work

- Improve radar model
  - Different basis functions (wavelets?)
  - Incorporate simple physics
- Incorporate correlation between pulses
- Experiment with new waveforms
- Achieve the promises of increased accuracy







Jicamarca, 51 us LFM chirp, 1 MHz bandwidth, 1 us sampling period

## SESS Radar Model Derivation



$$y(t) = \int_0^T \int_{-B/2}^{B/2} s(t - t_d) e^{2\pi i f_d(t - t_d)} e^{-2\pi i f_0 t_d} h(t_d, f_d) dt_d df_d$$

$$y(q\tau_s) = \sum_{k=1}^{rm} \int_{(k-1)\tau_b}^{k\tau_b} \sum_{p=-\frac{n}{2}+1}^{\frac{n}{2}} \int_{(p-1)\Delta f}^{p\Delta f} s(q\tau_s - t_d) e^{2\pi i f_d(q\tau_s - t_d)} e^{-2\pi i f_0 t_d} h(t_d, f_d) df_d dt_d$$

$$= \sum_{k,p} s_{rq-k+1} \int_{(k-1)\tau_b}^{k\tau_b} \int_{(p-1)\Delta f}^{p\Delta f} e^{2\pi i f_d q\tau_s} e^{-2\pi i (f_0 + f_d) t_d} h(t_d, f_d) df_d dt_d$$

$$=\sum_{k,p} s_{rq-k+1} e^{2\pi i p q \Delta f \tau_s} \int_{(k-1)\tau_b}^{k\tau_b} \int_{(p-1)\Delta f}^{p\Delta f} e^{2\pi i q \tau_s (f_d - p\Delta f)} e^{-2\pi i (f_0 + f_d) t_d} h(t_d, f_d) df_d dt_d$$

## SESS Radar Model Derivation



#### Want to write

as

$$y_q = \sum_{k,p} s_{rq-k+1} e^{2\pi i p q \Delta f \tau_s} \int_{(k-1)\tau_b}^{k\tau_b} \int_{(p-1)\Delta f}^{p\Delta f} e^{2\pi i q \tau_s (f_d - p\Delta f)} e^{-2\pi i (f_0 + f_d) t_d} h(t_d, f_d) df_d dt_d$$

$$y_q = \sum_{k=1}^{rm} s_{rq-k+1} \left( \sum_{p=0}^{n-1} e^{\frac{2\pi i p q}{n}} h_{p,k} \right)$$

#### • Approximate reflectivity

$$h_{p,k} \approx \int_{(k-1)\tau_b}^{k\tau_b} \int_{(p-1)\Delta f}^{p\Delta f} e^{2\pi i q \tau_s (f_d - p\Delta f)} e^{-2\pi i (f_0 + f_d) t_d} h(t_d, f_d) df_d dt_d$$

• Good for very small  $\Delta f$  or for point targets